

THERMAL IMPEDANCE MEASUREMENTS FOR  
INSULATED GATE BIPOLAR TRANSISTORS  
(DELTA GATE-EMITTER ON VOLTAGE METHOD)

1. Purpose. The purpose of this test method is to measure the thermal impedance of the IGBT under the specified conditions of applied voltage, current, and pulse duration. The temperature sensitivity of the gate-emitter ON voltage, under conditions of applied collector-emitter voltage and low emitter current, is used as the junction temperature indicator. This method is particularly suitable to enhancement mode, power IGBTs having relatively long thermal response times. This test method is used to measure the thermal response of the junction to a heating pulse. Specifically, the test may be used to measure dc thermal resistance and to ensure proper die mountdown to its case. This is accomplished through the appropriate choice of pulse duration and heat power magnitude. The appropriate test conditions and limits are detailed in 6.

2. Definitions. The following symbols and terms shall apply for the purpose of this test method:

- a.  $I_M$ : Emitter current applied during measurement of the gate-emitter ON voltage.
- b.  $I_H$ : Heating current through the collector or emitter lead.
- c.  $V_H$ : Heating voltage between the collector and emitter.
- d.  $P_H$ : Magnitude of the heating power pulse applied to DUT in watts; the product of  $I_H$  and  $V_H$ .
- e.  $t_H$ : Heating time during which  $P_H$  is applied.
- f.  $VTC$ : Voltage-temperature coefficient of  $V_{GE(ON)}$  with respect to  $T_J$ ; in mV/°C.
- g.  $K$ : Thermal calibration factor equal to reciprocal of  $VTC$ ; in °C/mV.
- h.  $T_J$ : Junction temperature in degrees Celsius.
  - $T_{Ji}$ : Junction temperature in degrees Celsius before start of the power pulse.
  - $T_{Jf}$ : Junction temperature in degrees Celsius at the end of the power pulse.
- i.  $T_X$ : Reference temperature in degrees Celsius.
  - $T_{Xi}$ : Initial reference temperature in degrees Celsius.
  - $T_{Xf}$ : Final reference temperature in degrees Celsius.
- j.  $V_{GE(ON)}$ : Gate-emitter ON voltage in millivolts.
  - $V_{GE(ON)i}$ : Initial gate-emitter ON voltage in millivolts.
  - $V_{GE(ON)f}$ : Final gate-emitter ON in millivolts.
- k.  $V_{GE(M)}$ : Gate-emitter voltage during measurement periods.
  - $V_{GE(H)}$ : Gate-emitter voltage during heating periods.
- l.  $V_{CE(M)}$ : Collector-emitter voltage during measurement periods.
  - $V_{CE(H)}$ : Collector-emitter voltage during heating periods.
- m.  $V_{CG}$ : Collector-gate voltage, adjusted to provide appropriate  $V_{CE}$ .

- n.  $t_{MD}$ : Measurement delay time is defined as the time from the removal of heating power  $P_H$  to the start of the  $V_{GE(ON)}$  measurement.
- o.  $t_{SW}$ : Sample window time during which final  $V_{GE(ON)}$  measurement is made.
- p.  $Z_{\Theta JX}$ : Transient junction-to-reference point thermal impedance in  $^{\circ}C/W$ .  $Z_{\Theta JX}$  or specified power pulse duration is:

$$Z_{\Theta JX} = \left( T_{jF} - T_{jI} - \frac{\Delta T_x}{P_H} \right)$$

Where:  $\Delta T_x$  = change in reference point temperature during the heating pulse (see 5.2 and 5.4 for short heating pulses, e.g., die attach evaluation, this term is normally negligible.)

3. Apparatus. The apparatus required for this test shall include the following as applicable to the specified test procedure.

3.1 Case temperature measurement. A thermocouple for measuring the case temperature at a specified reference point. The recommended reference point shall be located on the case under the heat source. Thermocouple material shall be copper- constantan (type T) or equivalent. The wire size shall be no larger than AWG size 30. The junction of the thermocouple shall be welded, rather than soldered or twisted, to form a bead. The accuracy of the thermocouple and its associated measuring system shall be  $\pm 0.5^{\circ}C$ . Proper mounting of the thermocouple to ensure intimate contact to the reference point is critical for system accuracy.

3.2 Controlled temperature environment. A controlled temperature environment capable of maintaining the case temperature during the device calibration procedure to within  $\pm 1^{\circ}C$  over the temperature range of  $+23^{\circ}C$  to  $+100^{\circ}C$ , the recommended temperatures for measuring K-factor.

3.3 K factor calibration. A K factor calibration setup, as shown on figure 3103-1, that measures  $V_{GE(ON)}$  for the specified values of  $V_{CE}$  and  $I_M$  in an environment where temperature is both controlled and measured. A temperature controlled circulating fluid bath is recommended. The current source must be capable of supplying  $I_M$  with an accuracy of  $\pm 2$  percent. The voltage source  $V_{CG}$  is adjusted to supply  $V_{CE}$  with an accuracy of  $\pm 2$  percent. The voltage measurement of  $V_{GE(ON)}$  shall be made with a voltmeter capable of 1 mV resolution. The device-to-current source wire size shall be sufficient to handle the measurement current (AWG size 22 stranded is typically used for up to 100 mA).

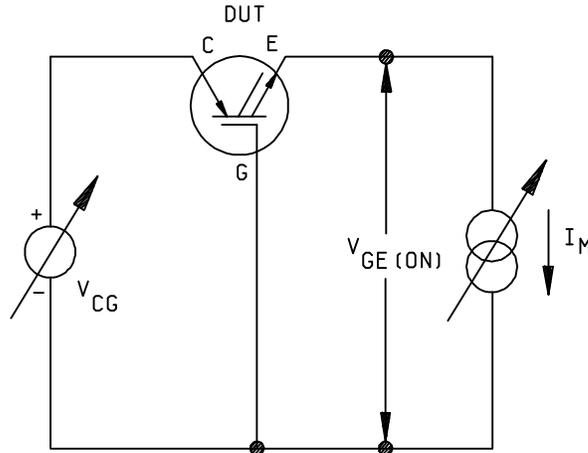


FIGURE 3103-1. K factor calibration setup.

3.4 Thermal testing. There are two approaches to the actual thermal testing, either the common-gate or the common-source method. Both methods work equally well, although the common-source method may be more reliable and less potentially damaging to the DUT. The figures and description below describe the thermal measurement for n-channel enhancement mode devices. Opposite polarity devices can be tested by appropriately reversing the various supplies. Depletion mode devices can be tested by applying the gate-emitter voltage ( $V_{GE}$ ) in the appropriate manner.

3.4.1 Common-gate thermal test circuit. A common-gate configuration test circuit used to control the device and to measure the temperature using the gate-emitter ON voltage as the temperature sensing parameter as shown on figure 3103-2. Polarities shown are for n-channel devices but the circuit may be used for p-channel types by reversing the polarities of the voltage and current sources.

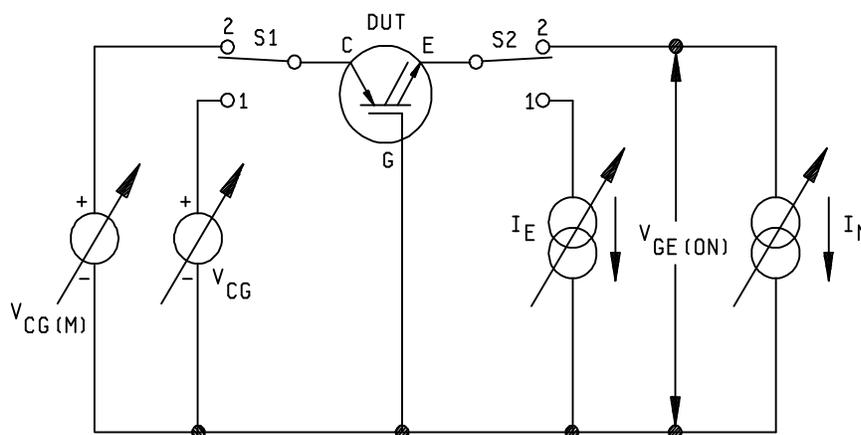
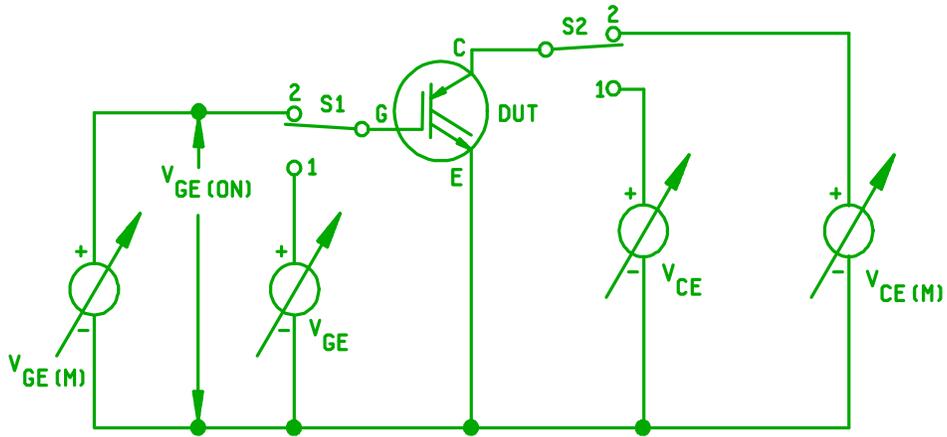


FIGURE 3103-2. Common-gate thermal impedance measurement circuit (gate-emitter on voltage method).

The circuit consists of the DUT, two voltage sources, two current sources, and two electronic switches. During the heating phase of the measurement, switches S1 and S2 are in position 1. The values of  $V_{CG}$  and  $I_E$  are adjusted to achieve the desired values of  $I_C$  and  $V_{CE}$  for the  $P_H$  "heating" condition.

To measure the initial and post heating pulse junction temperatures of the DUT, switches S1 and S2 are each switched to position 2. This puts the gate at the measurement voltage level  $V_{CG(M)}$  and connects the current source  $I_M$  to supply measurement current to the emitter. The values of  $V_{CG(M)}$  and  $I_M$  must be the same as used in the K factor calibration if actual junction temperature rise data is required. Figures 3103-4 and 3103-5 show the waveforms associated with the three segments of the test.

3.4.2 Common-source thermal test circuit. A common-source configuration test circuit used to control the device and to measure the temperature using the gate-emitter ON voltage as the temperature sensing parameter as shown on figure 3103-3. Polarities shown are for n-channel devices but the circuit may be used for p-channel types by reversing the polarities of the voltage and current sources.



NOTE: The circuit consists of the DUT, four voltage sources, and two electronic switches. During the heating phase of the measurement, switches S1 and S2 are in position 1. The values of  $V_{CE}$  and  $V_{GE}$  are adjusted to achieve the desired values of  $I_C$  and  $V_{CE}$  for the PH "heating" condition.

FIGURE 3103-3. Common-source thermal impedance measurement circuit (gate-emitter on voltage method).

To measure the initial and post heating pulse junction temperatures of the DUT, switches S1 and S2 are each switched to position 2. This puts the collector at the measurement voltage level  $V_{CE(M)}$  and the gate at  $V_{GE(M)}$ , which must be adjusted to obtain  $I_M$ . The values of  $V_{CE(M)}$  and  $I_M$  must be the same as used in the K factor calibration if actual junction temperature rise data is required. Figures 3103-4 and 3103-5 show the waveforms associated with the three segments of the test.

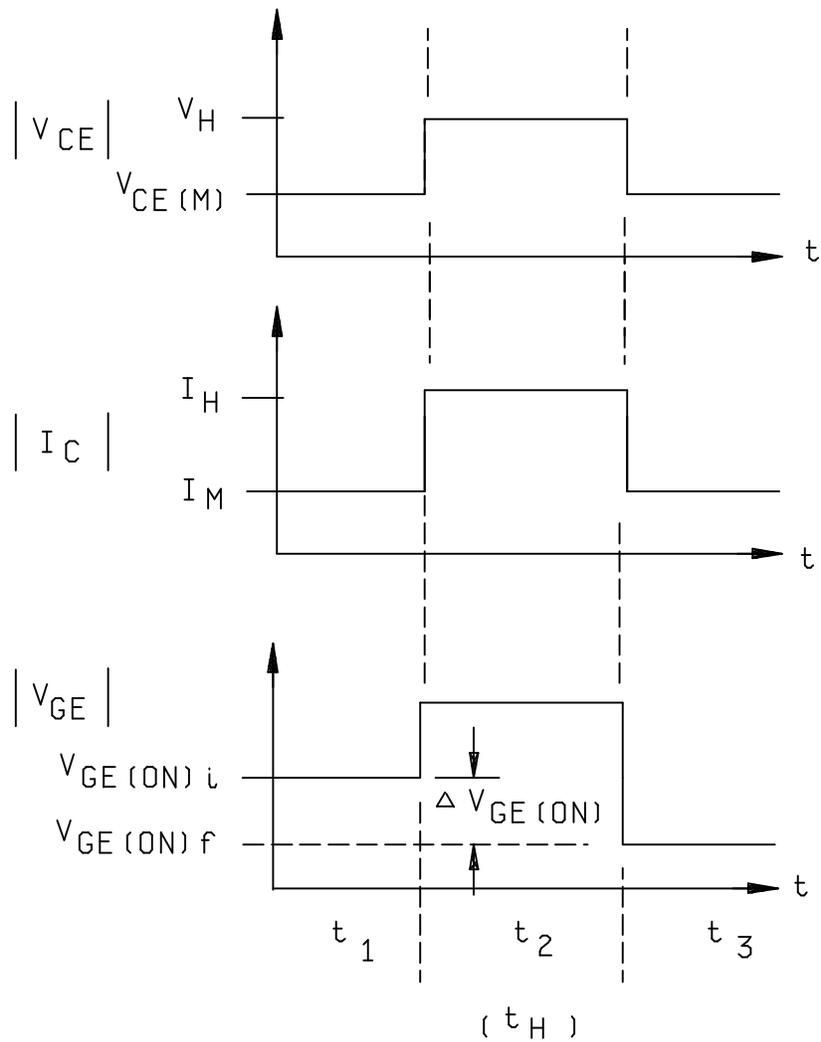


FIGURE 3103-4. Device waveforms during the three segments of the thermal transient test.

The value of  $t_{MD}$  is critical to the accuracy of the measurement and must be properly specified in order to ensure measurement repeatability. Note that some test equipment manufacturers include the sample and hold window time  $t_{SW}$  within their  $t_{MD}$  specification.

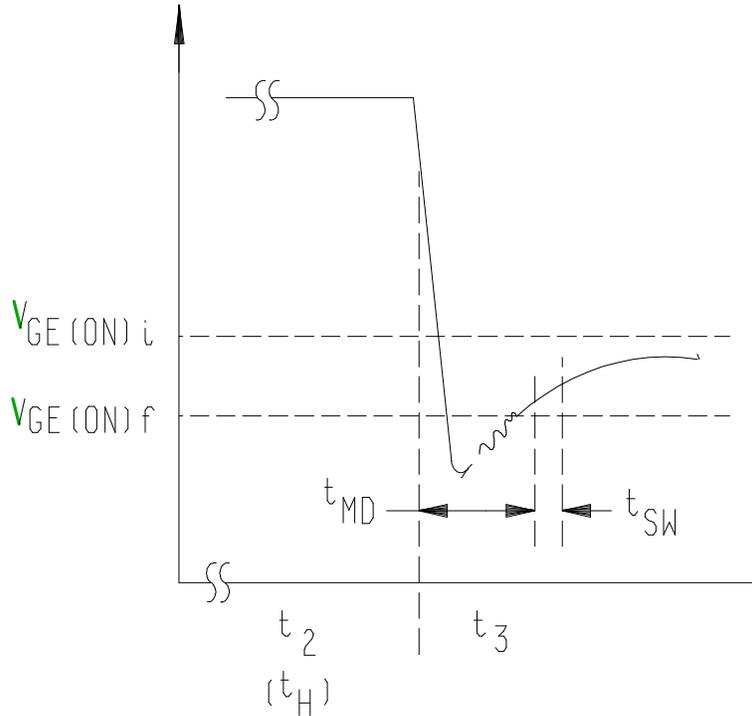


FIGURE 3103-5. Second  $V_{GE}$  measurement waveform.

NOTE: The circuits for both common-gate and common-source thermal measurements can be modified so that  $V_{CE}$  is applied during both measurement and heating periods if the value of  $V_{CE}$  is at least ten times the value of  $V_{GE(ON)}$ . Further, the common-gate circuit can be modified so that  $I_M$  is continually applied as long as the  $I_E$  current source can be adjusted for the desired value of heating current.

3.5 Source-drain forward voltage. Suitable sample-and-hold voltmeter or oscilloscope to measure source-drain forward voltage at specified times.  $V_{GE(ON)}$  shall be measured to within 5 mV, or within 5 percent of  $(V_{GE(ON)i} - V_{GE(ON)f})$ , whichever is less.

4. Measurement of the TSP. The required calibration of  $V_{GE(ON)}$  versus  $T_J$  is accomplished by monitoring  $V_{GE(ON)}$  for the required values of  $V_{CE}$  and  $I_M$  as the heat sink temperature (and thus the DUT temperature) is varied by external heating. The magnitudes of  $V_{CE}$  and  $I_M$  shall be chosen so that  $V_{GE(ON)}$  is a linearly decreasing function over the expected range of  $T_J$  during the power pulse. For this condition,  $V_{CE}$  must be at least three times  $V_{GE(ON)}$ .  $I_M$  must be large enough to ensure that the device is turned on but not so large as to cause any significant self-heating. (This will normally be 1 mA for low power devices and up to 100 mA for high power ones.) An example calibration curve is shown on figure 3103-6.

4.1 K factor calibration. A calibration factor K (which is the reciprocal of VTC or the slope of the curve on figure 3103-4) can be defined as:

$$K = \frac{I}{VTC} = \left| \frac{T_{J1} - T_{J2}}{V_{GE(ON)1} - V_{GE(ON)2}} \right| \text{ } ^\circ\text{C}/\text{mV}$$

It has been found experimentally that the K-factor variation for all devices within a given device type class is small. The usual procedure is to perform a K factor calibration on a 10 to 12 piece sample from a device lot and determine the average K and standard deviation ( $\sigma K$ ). If  $\sigma K$  is less than or equal to three percent of the average value of K, then the average value of K can be used for all devices within the lot. If  $\sigma K$  is greater than three percent of the average value of K, then all the devices in the lot shall be calibrated and the individual values of K shall be used in thermal impedance calculations or in correcting  $\Delta V_{GE(ON)}$  values for comparison purposes.

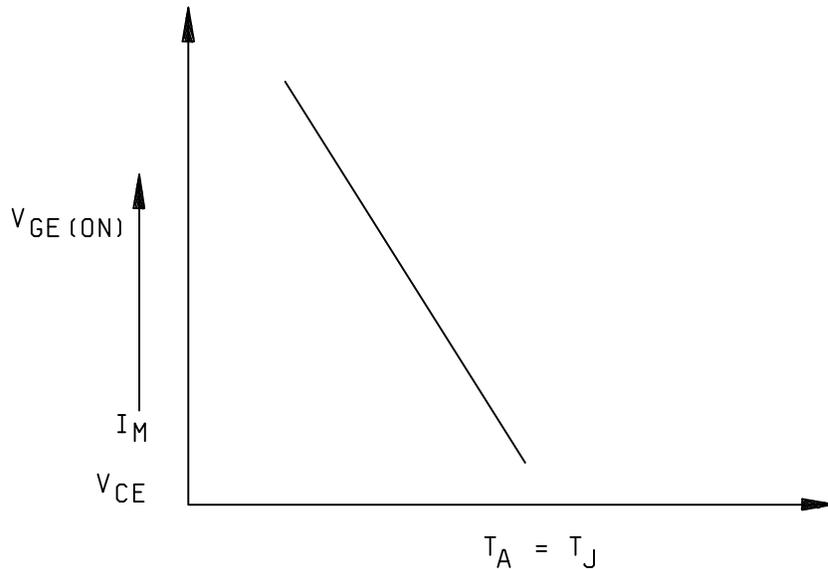


FIGURE 3103-6. Example curve of  $V_{GE(ON)}$  versus  $T_J$ .

When screening to ensure proper die attachment within a given lot, this calibration step is not required, (e.g., devices of a single manufacturer with identical PIN and case style). In such cases, the measure of thermal response may be  $\Delta V_{GE(ON)}$  for a short heating pulse, and the computation of  $\Delta T_J$  or  $Z_{\Theta JX}$  is not necessary. (For this purpose,  $t_H$  shall be 10 ms for TO-39 size packages and 100 ms for TO-3 packages.)

5. Calibration. K factor must be determined according to the procedure outlined in 4, except as noted in 4.1.

5.1 Reference point temperature. The reference point is usually chosen to be on the bottom of the transistor case directly below the semiconductor chip in a TO-204 metal can or in close proximity to the chip in other styles of packages. Reference temperature point location must be specified and its temperature shall be monitored using the thermocouple mentioned in 3.1 during the preliminary testing. If it is ascertained that  $T_X$  increases by more than five percent of measured junction temperature rise during the power pulse, then either the heating power pulse magnitude must be decreased, the DUT must be mounted in a temperature controlled heat sink, or the calculated value of thermal impedance must be corrected to take into account the thermal impedance of the reference point to the cooling medium or heat sink.

Temperature measurements for monitoring, controlling or correcting reference point temperature changes are not required if the  $t_H$  value is low enough to ensure that the heat generated within the DUT has not had time to propagate through the package. Typical values of  $t_H$  for this case are in the 10 ms to 500 ms range, depending on DUT package type and material.

5.2 Thermal measurements. The following sequence of tests and measurements must be made.

- a. Prior to the power pulse:
  - (1) Establish reference point temperature  $T_{X_i}$ .
  - (2) Apply measurement voltage  $V_{CE}$ .
  - (3) Apply measurement current  $I_M$ .
  - (4) Measure gate-emitter ON voltage  $V_{GE(ON)_i}$  (a measurement of the initial junction temperature).

- b. Heating pulse parameters:
  - (1) Apply collector-emitter heating voltage  $V_H$ .
  - (2) Apply collector heating current  $I_H$  as required by adjustment of gate-emitter voltage.
  - (3) Allow heating condition to exist for the required heating pulse duration  $t_H$ .
  - (4) Measure reference point temperature  $T_{X_f}$  at the end of heating pulse duration.

NOTE:  $T_X$  measurements are not required if the  $t_H$  value meets the requirements stated in 5.2.

- c. Post power pulse measurements:
  - (1) Apply measurement current  $I_M$ .
  - (2) Apply measurement voltage  $V_{CE}$ .
  - (3) Measure gate-emitter ON voltage  $V_{GE(ON)_f}$  (a measurement of the final junction temperature).
  - (4) Time delay between the end of the power pulse and the completion of the  $V_{GE(ON)_f}$  measurement as defined by the waveform of figure 3103-4 in terms of  $t_{MD}$  plus  $t_{SW}$ .
- d. The value of thermal impedance,  $Z_{\Theta JX}$ , is calculated from the following formula:

$$Z_{\Theta JX} = \frac{\Delta T_J}{P_H} = \left| \frac{K (V_{GE(ON)_f} - V_{GE(ON)_i})}{(I_H)(V_H)} \right| \circ C / W$$

This value of thermal impedance will have to be corrected if  $T_{X_f}$  is greater than  $T_{X_i}$  by  $+5^\circ C$ . The correction consists of subtracting the component of thermal impedance due to the thermal impedance from the reference point (typically the device case) to the cooling medium or heat sink.  $T_X$  measurements are not required if the  $t_H$  value meets the requirements stated in 5.2.

This thermal impedance component has a value calculated as follows:

$$Z_{\theta X-HS} = \frac{\Delta T_X}{P_H} = \frac{(T_{Xf} - T_{Xi})}{(I_H)(V_H)}$$

Where: HS = cooling medium or heat sink (if used).

Then:

$$Z_{\theta JX} = Z_{\theta JX} - Z_{\theta X-HS}$$

|  
Corrected

|  
Calculated

NOTE: This last step is not necessary for die attach evaluation (see 4.1).

6. Test conditions and measurements to be specified and recorded.

6.1 K factor calibration.

6.1.1 Test conditions. Specify the following test conditions:

- a.  $I_M$  current magnitude \_\_\_\_\_mA  
(See detail specification for current value)
- b.  $V_{CE}$  voltage magnitude \_\_\_\_\_V  
(See detail specification for voltage value)
- c. Initial junction temperature \_\_\_\_\_°C  
(Normally +25°C ±5°C)
- d. Final junction temperature \_\_\_\_\_°C  
(Normally +100°C ±10°C)

6.1.2 Data. Record the following data:

- a. Initial  $V_{GE(ON)}$  voltage \_\_\_\_\_mV
- b. Final  $V_{GE(ON)}$  voltage \_\_\_\_\_mV

6.1.3 K factor. Calculate K factor in accordance with the following equation:

$$K = \left| \frac{T_{J1} - T_{J2}}{V_{GE(ON)1} - V_{GE(ON)2}} \right| \text{ } ^\circ\text{C} / \text{mV}$$

6.1.4 For die attachment evaluation, this step may not be necessary (see 4.1).

6.2 Thermal impedance measurements.6.2.1 Test conditions. Specify the following test conditions:

- a.  $I_M$  measuring current \_\_\_\_\_mA  
(Must be same as used for K factor calibration)
- b.  $V_{CE}$  measuring voltage \_\_\_\_\_V  
(Must be same as used for K factor calibration)
- c.  $I_H$  heating current \_\_\_\_\_A
- d.  $V_H$  collector-emitter heating voltage \_\_\_\_\_V
- e.  $t_H$  heating time \_\_\_\_\_s
- f.  $t_{MD}$  measurement time delay \_\_\_\_\_ $\mu$ s
- g.  $t_{SW}$  sample window time \_\_\_\_\_ $\mu$ s

(NOTE:  $I_H$  and  $V_H$  are usually chosen so that  $P_H$  is approximately two-thirds of device rated power dissipation.)

6.2.2 Data. Record the following data:

- a.  $T_{X_i}$  initial reference temperature \_\_\_\_\_ $^{\circ}$ C
- b.  $T_{X_f}$  final reference temperature \_\_\_\_\_ $^{\circ}$ C

6.2.2.1  $\Delta V_{GE(ON)}$  data:

$\Delta V_{GE(ON)}$  \_\_\_\_\_mV

6.2.2.2  $V_{GE(ON)}$  data:

- a.  $V_{GE(ON)_i}$  initial source-drain voltage \_\_\_\_\_V
- b.  $V_{GE(ON)_f}$  final source-drain voltage \_\_\_\_\_V

$T_X$  measurements are not required if the  $t_H$  value meets the requirements stated in 5.2.

6.2.3 Thermal impedance. Calculate thermal impedance using the procedure and equations shown in 5.4.

6.3  $\Delta V_{GE(ON)}$  measurements for screening. These measurements are made for  $t_H$  values that meet the intent of 4.1 and the requirements stated in 5.2.

6.3.1 Test conditions. Specify the following test conditions:

- a.  $I_M$  measuring current \_\_\_\_\_mA
- b.  $V_{GE}$  measuring voltage \_\_\_\_\_V
- c.  $I_H$  heating current \_\_\_\_\_A
- d.  $V_H$  collector-emitter heating voltage \_\_\_\_\_V
- e.  $t_H$  heating time \_\_\_\_\_s

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f.  $t_{MD}$  measurement time delay \_\_\_\_\_ $\mu$ s

g.  $t_{SW}$  sample window time \_\_\_\_\_ $\mu$ s

(The values of  $I_H$  and  $V_H$  are usually chosen equal to or greater than the values used for thermal impedance measurements.)

6.3.2 Specified limits. The following data is compared to the specified limits:

6.3.2.1  $\Delta V_{GE(ON)}$  data:

$\Delta V_{GE(ON)}$  \_\_\_\_\_mV

6.3.2.2  $V_{GE(ON)}$  data:

a.  $V_{GE(ON)i}$  initial source-drain voltage \_\_\_\_\_V

b.  $V_{GE(ON)f}$  final source-drain voltage \_\_\_\_\_V

Compute  $\Delta V_{GE(ON)}$  \_\_\_\_\_mV

6.3.2.3  $\Delta T_J$  calculation. Optionally calculate  $\Delta T_J$  if the K factor results produce a  $\sigma$  greater than three percent of the average value of K.

$$\Delta T_J = K(\Delta V_{GE(ON)}) \text{ } ^\circ\text{C}$$